

# Method for Reconstruction of Electrical Properties inside Human Bodies using MRI

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# Background

- **Electrical conductivity and permittivity imaging** inside the human body  
⇒ pathological information: breast carcinoma (tumor) exhibits conductivity changes up to a factor of 10. [Katscher, 2009]
- ⇒ Small tumor/cancer tissues can be detected

## ■ Diagnosis of malignant tissue [Joines *et al.*, 1994]

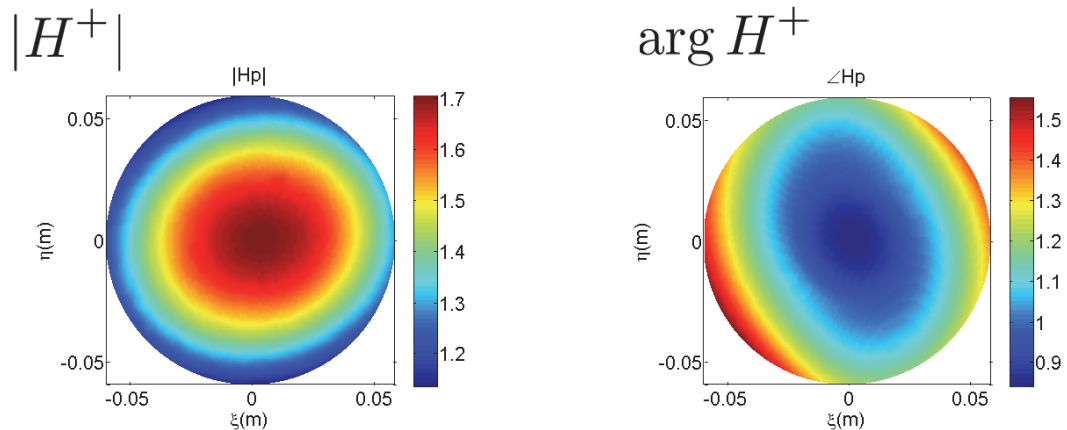
Tissue	$\sigma_{\text{normal}}$	$\sigma_{\text{malignant}}$	$\epsilon_{r,\text{normal}}$	$\epsilon_{r,\text{malignant}}$
Liver	0.49	0.66	62	66
Lung	0.49	0.82	77	69
Mammal	0.11	<b>0.78</b>	21	<b>69</b>

# Magnetic resonance electrical property tomography (MREPT)



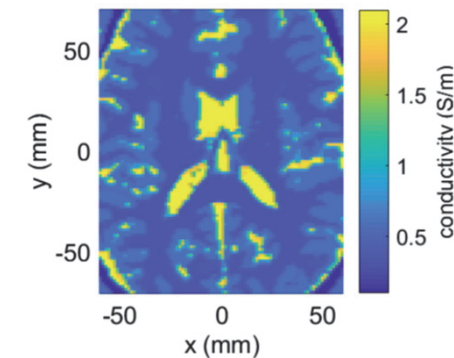
'Birdcage coil' generates the rotating magnetic field with a frequency of e.g. 128MHz

What is measured: magnetic field inside the body



What should be reconstructed:

Electric conductivity and permittivity



# Governing equation: time-harmonic Maxwell's equations

$$\left\{ \begin{array}{ll} \text{Faraday's law} & \nabla \times \mathbf{E} = -i\omega\mu_0\mathbf{H} \\ \text{Ampere's law} & \nabla \times \mathbf{H} = \gamma\mathbf{E} + \mathbf{J} \\ \text{Silver-Muller} & \\ \text{radiation condition} & \lim_{|\mathbf{r}| \rightarrow \infty} (\mathbf{H} \times \mathbf{r} - |\mathbf{r}|\mathbf{E}) = \mathbf{0} \end{array} \right.$$

$$\gamma = \boxed{\sigma} + i\omega\boxed{\epsilon} \quad : \text{admittivity}$$

conductivity    permittivity

MREPT inverse problem: given  $H^+ = \frac{1}{2}(H_x + iH_y)$  inside the body  $D$ ,  
reconstruct  $\gamma = \sigma + i\omega\epsilon$ .

# Conventional method

$$\left\{ \begin{array}{l} \nabla \times \mathbf{E} = -i\omega\mu_0\mathbf{H} \\ \nabla \times \mathbf{H} = \gamma\mathbf{E} \end{array} \right. \quad \text{in } D$$

Katscher,  
IEEE Tr. Medical Imaging,  
2009.

By eliminating  $\mathbf{E}$ , a non-linear PDE for  $\gamma$  is obtained:

$$(\nabla \times \mathbf{H}) \times \frac{\nabla\gamma}{\gamma} + i\omega\mu_0\mathbf{H}\gamma = \Delta\mathbf{H}$$

By neglecting  $\nabla\gamma$ , a reconstruction formula is obtained:

$$\gamma = \frac{\Delta H^+}{i\omega\mu_0 H^+}$$

# Objective

Derivation of an **explicit** reconstruction formula for inhomogeneous admittivity  $\gamma$  from the measured magnetic field  $H^+$

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1. Derivation of a direct reconstruction formula for the 2D problem
2. Extension to the 3D problem

# 1. Derivation of a direct reconstruction formula

Assumptions:

$$\left\{ \begin{array}{l} 1) \ H_z = 0 \\ 2) \ \partial_z H^+ = 0 \end{array} \right. \quad \begin{array}{l} \text{Usual assumptions from the structure} \\ \text{of 'birdcage coils' aligned along the z-axis} \\ \gamma \text{ does not change w.r.t the z-axis} \end{array}$$

- First, we consider the 2D problem and derive a direct reconstruction formula.
- Second, we remove Assumption 2) and propose an iterative algorithm.

# Dbar equations derived from time-harmonic Maxwell's equations

Define the complex derivatives:  $\partial \equiv \frac{1}{2}(\partial_x - i\partial_y)$ ,  $\bar{\partial} \equiv \frac{1}{2}(\partial_x + i\partial_y)$

Let  $H^+ \equiv \frac{1}{2}(H_x + iH_y)$ ,  $E^+ \equiv \frac{1}{2}(E_x + iE_y)$

Then, under the two assumptions, Maxwell's equations in  $D$  are written:

$$\left\{ \begin{array}{ll} \partial H^+ = \frac{i\gamma}{4} E_z & \text{Ampere's law} \\ \bar{\partial} E_z = \omega\mu_0 H^+ & \text{Faraday's law} \end{array} \right.$$



Ampere's law

$$4\partial H^+ = i\gamma E_z$$



$$\gamma = \frac{4\partial H^+}{iE_z}$$

Complex derivative of the measured magnetic field

z-component of the electric field



Faraday's law

**Dbar equation**

$$\bar{\partial} E_z = \omega\mu_0 H^+$$

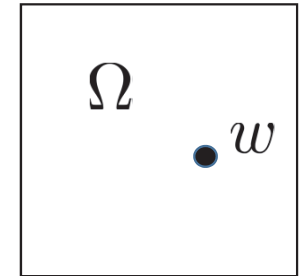
We use Faraday's equation to represent  $E_z$  in terms of  $H^+$

# Generalized Cauchy formula for Dbar equations

- $f \in C^1(\Omega) \cap C(\bar{\Omega})$  ,  $\Omega$ : domain bounded by a Jordan contour
- $f$  satisfies a Dbar equation:  $\bar{\partial}f = g$  (inhomogeneous Cauchy-Riemann system)

➔ Generalized Cauchy formula

$$f(w) = \frac{1}{2\pi i} \int_{\partial\Omega} \frac{f(\zeta)}{\zeta - w} d\zeta - \frac{1}{\pi} \int \int_{\Omega} \frac{g(\zeta)}{\zeta - w} d\xi d\eta, \quad w \in \Omega$$



Faraday's law  $\bar{\partial}E_z = \omega\mu_0 H^+$       **Dbar equation**

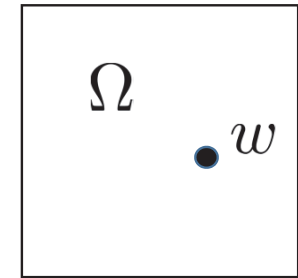
➔ The z-component of the electric field can be expressed as

$$E_z(w) = \frac{1}{2\pi i} \int_{\partial\Omega} \frac{E_z(\zeta)}{\zeta - w} d\zeta - \frac{\omega\mu_0}{\pi} \int \int_{\Omega} \frac{H^+(\zeta)}{\zeta - w} d\xi d\eta, \quad w \in \Omega$$

$$E_z(w) = \frac{1}{2\pi i} \int_{\partial\Omega} \frac{E_z(\zeta)}{\zeta - w} d\zeta - \frac{\omega\mu_0}{\pi} \int \int_{\Omega} \frac{H^+(\zeta)}{\zeta - w} d\xi d\eta, \quad w \in \Omega$$

Ampere's law  $4\partial H^+ = i\gamma E_z$

$$\frac{4\partial H^+}{i\gamma}$$



If we give the boundary value of  $\gamma$ , the electric field  $E_z$  can be computed.

By substituting this into

$$\gamma(w) = \frac{4\partial H^+(w)}{iE_z(w)}$$

we arrive at the explicit reconstruction formula:

## Direct reconstruction formula of the admittivity $\gamma$

Given  $H^+$  in  $\Omega$  and  $\gamma$  on  $\partial\Omega$ ,

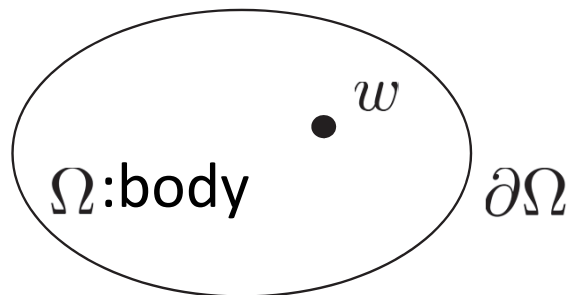
the admittivity at an arbitrary point  $w \in \Omega$  is reconstructed by

$$\gamma(w) = \frac{4\pi i \partial H^+(w)}{\int_{\partial\Omega} \frac{\frac{2}{\gamma(\zeta)} \partial H^+(\zeta)}{\zeta - w} d\zeta + \omega \mu_0 \int_{\Omega} \frac{H^+(\zeta)}{\zeta - w} d\xi d\eta}$$

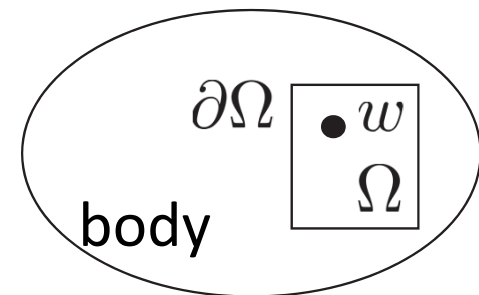
# How to give the boundary value of $\gamma$

$$\gamma(w) = \frac{4\pi i \partial H^+(w)}{\int_{\partial\Omega} \frac{\gamma(\zeta) \partial H^+(\zeta)}{\zeta - w} d\zeta + \omega \mu_0 \int_{\Omega} \frac{H^+(\zeta)}{\zeta - w} d\xi d\eta}$$

Scenario 1: Take  $\Omega$  as a whole body  $D$  and measure  $\gamma$  near the body surface

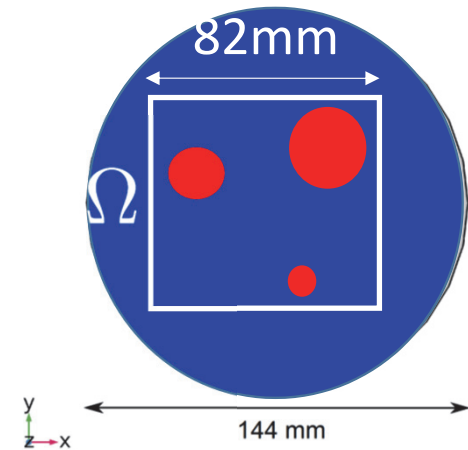


Scenario 2: Take  $\Omega$  as a local domain inside which a small cancer may exist and give a normal value of  $\gamma$  on  $\partial\Omega$



# Numerical simulations

- Three cylinders (conductivity = 1S/m, diameters = 10mm, 20mm, 30mm) in a cylinder (conductivity = 0.5 S/m).
- Forward solution was computed by an FEM software (COMSOL).  
f=123MHz (corresponding to 2.89T)
- $\Omega$  : 82mm x 82mm
- Discretization: pixel size = 1.4mm x 1.4mm



- Singular integral  $\int \int_{U_\epsilon(w)} \frac{H^+(\zeta)}{\zeta - w} d\xi d\eta = 0$

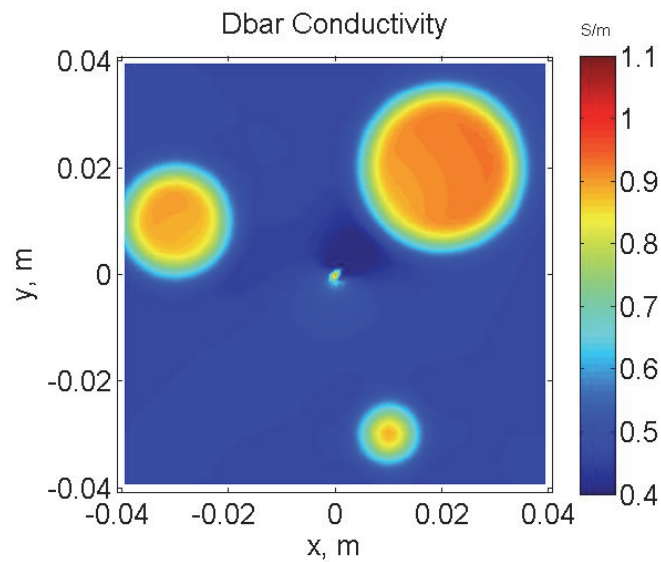
$$\longrightarrow \int \int_{\Omega} \frac{H^+(\zeta)}{\zeta - w} d\xi d\eta \simeq \int \int_{\Omega/\{w\}} \frac{H^+(\zeta)}{\zeta - w} d\xi d\eta$$

- For computation of  $\partial H^+$  and  $\Delta H^+$ ,  
Gaussian filter + Savitzky-Golay Filter were used.  
(2<sup>nd</sup> degree polynomial approximation)

$$\gamma(w) = \frac{4\pi i \partial H^+(w)}{\int_{\partial\Omega} \frac{\frac{2}{\gamma(\zeta)} \partial H^+(\zeta)}{\zeta - w} d\zeta + \omega \mu_0 \int \int_{\Omega} \frac{H^+(\zeta)}{\zeta - w} d\xi d\eta}$$

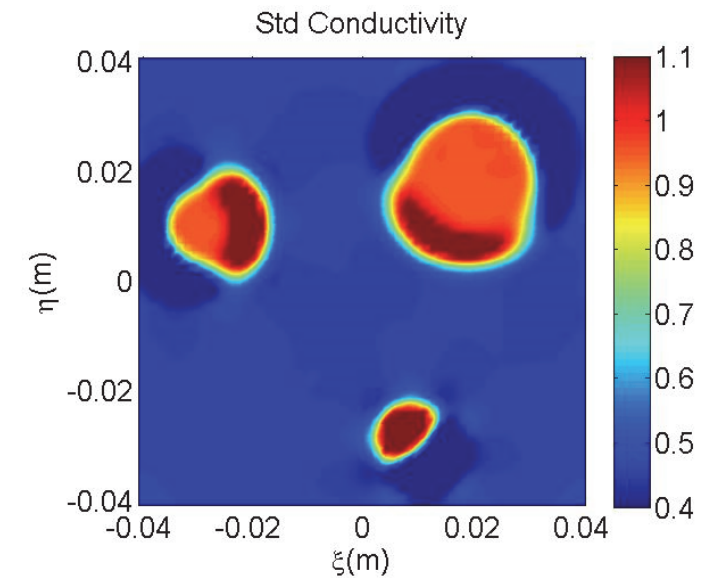
# Reconstruction (noiseless)

## Proposed



The three domains were well reconstructed.

## Conventional (standard)

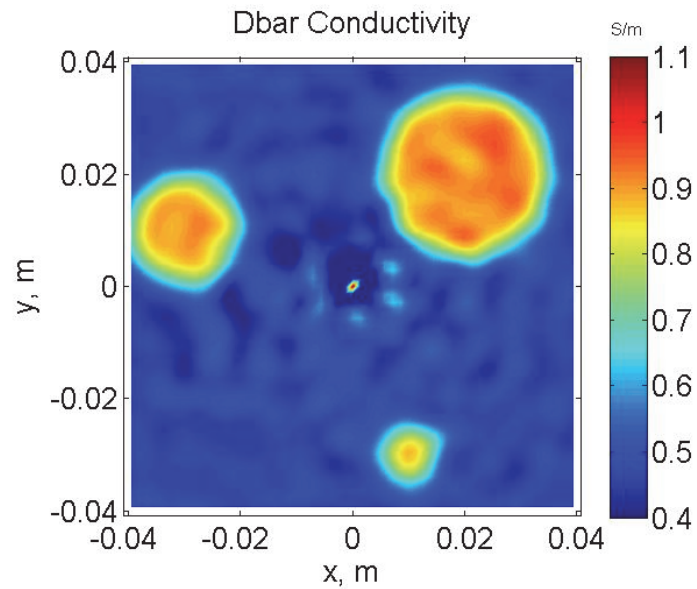


The large errors were observed at the boundary.

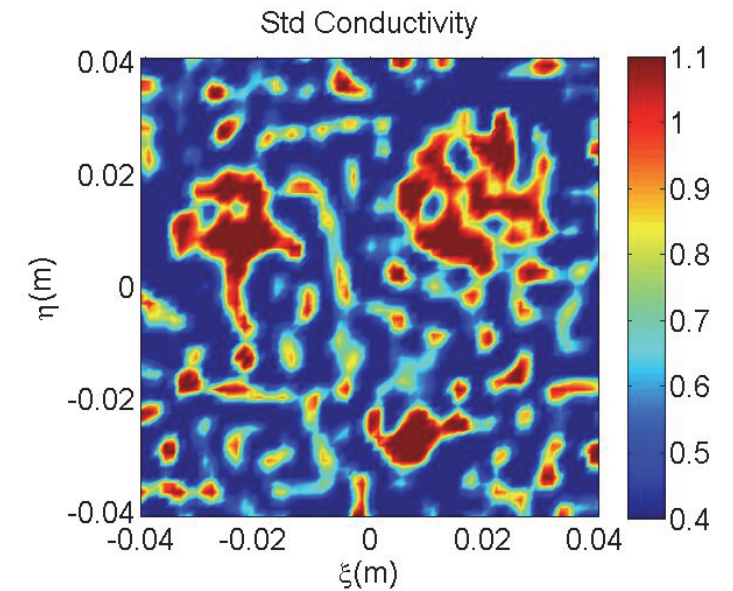


# Reconstruction (1%noise)

Proposed



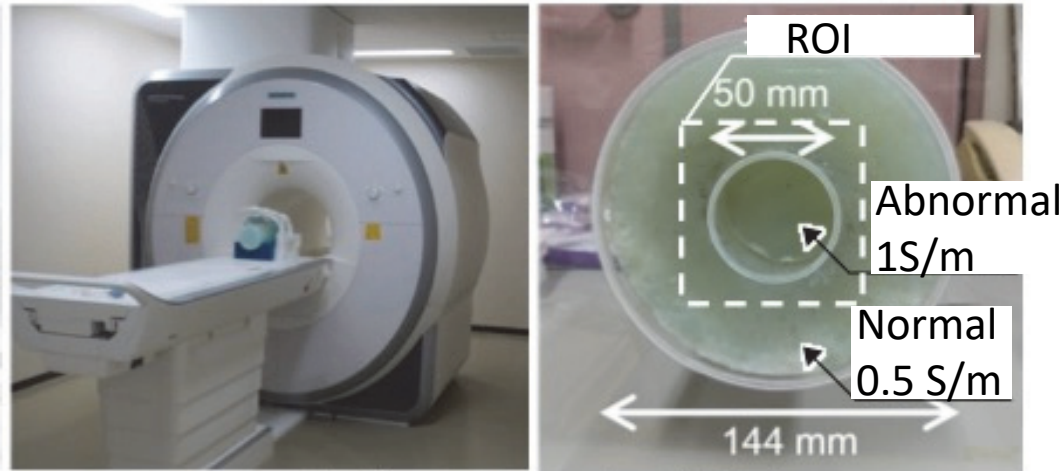
Conventional (standard)



$$\gamma(w) = \frac{4\pi i \partial H^+(w)}{\int_{\Gamma} \frac{\frac{2}{\gamma(\zeta)} \partial H^+(\zeta)}{\zeta - w} d\zeta + \omega \mu_0 \int \int_{\Omega} \frac{H^+(\zeta)}{\zeta - w} d\xi d\eta}$$

$$\gamma = \frac{\Delta H^+}{i\omega \mu_0 H^+}$$

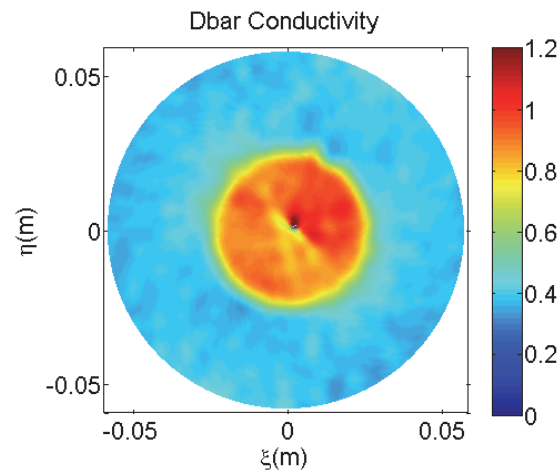
# Phantom experiments



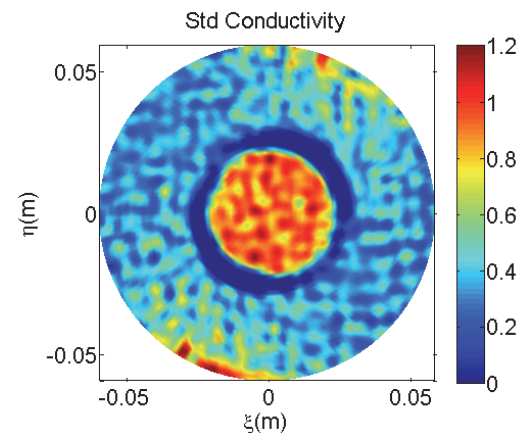
3T MRI

Phantom

## Proposed



## Conventional (standard)



- discontinuous jump of the conductivity
- robustness against noise

## 2. Extension to the 3D problem

Assumptions:

- |   |                         |   |
|---|-------------------------|---|
| { | 1) $H_z = 0$            | Usual assumptions from the structure of 'birdcage coils'        |
|   | 2) $\partial_z H^+ = 0$ | <del><math>\gamma</math> does not change w.r.t the z-axis</del> |

{	Ampere's law (z-compnents) + $i \nabla \cdot \mathbf{H} = 0$	$4i\partial H^+ = \gamma E_z$
	Ampere's law (xy-compnent)	$-\partial_z H^+ = i\gamma E^+$
	Faraday's law (xy-compnents)	$\bar{\partial} E_z - \partial_z E^+ = \omega \mu_0 H^+$

## Extension without the assumption $\partial_z H^+ = 0$

The Dbar equation is changed to:  $\bar{\partial} E_z = \omega \mu_0 H^+ + \partial_z E^+$

Iterative Algorithm:

1) Use the direct reconstruction formula to obtain an initial estimate.

2) Compute  $E^+ = \frac{i\partial_z H^+}{\gamma}$  with the reconstructed  $\gamma$ .

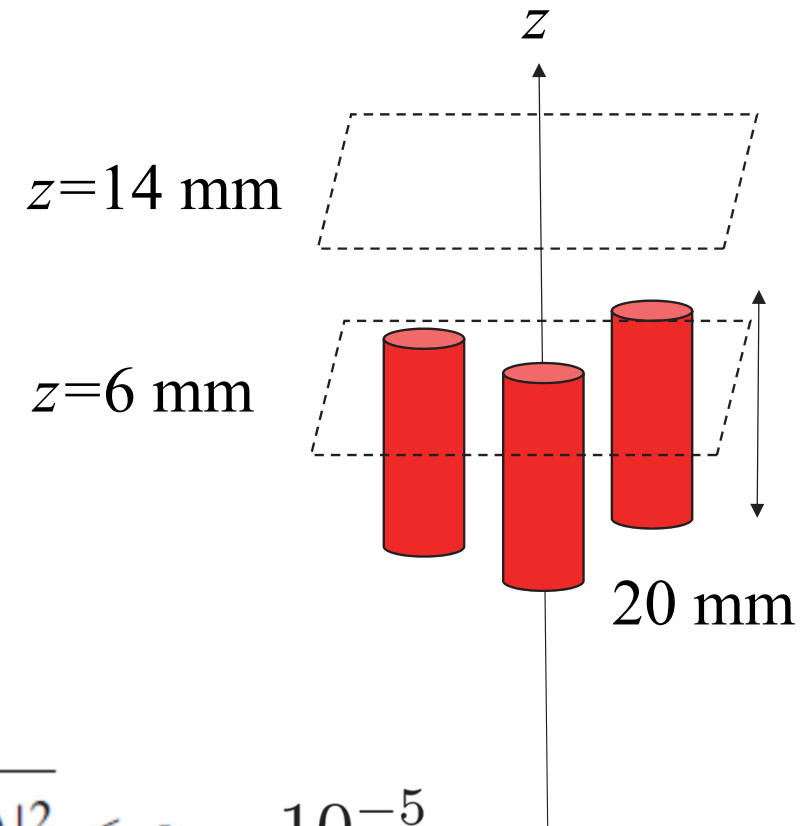
3) 
$$\gamma(w) = \frac{4\pi i \partial H^+(w)}{\int_{\Gamma} \frac{\partial H^+}{\zeta - w} d\zeta + \int \int_{\Omega} \frac{\omega \mu_0 H^+(\zeta) + \partial_z E^+(\zeta)}{\zeta - w} d\xi d\eta}$$

Go to 2).

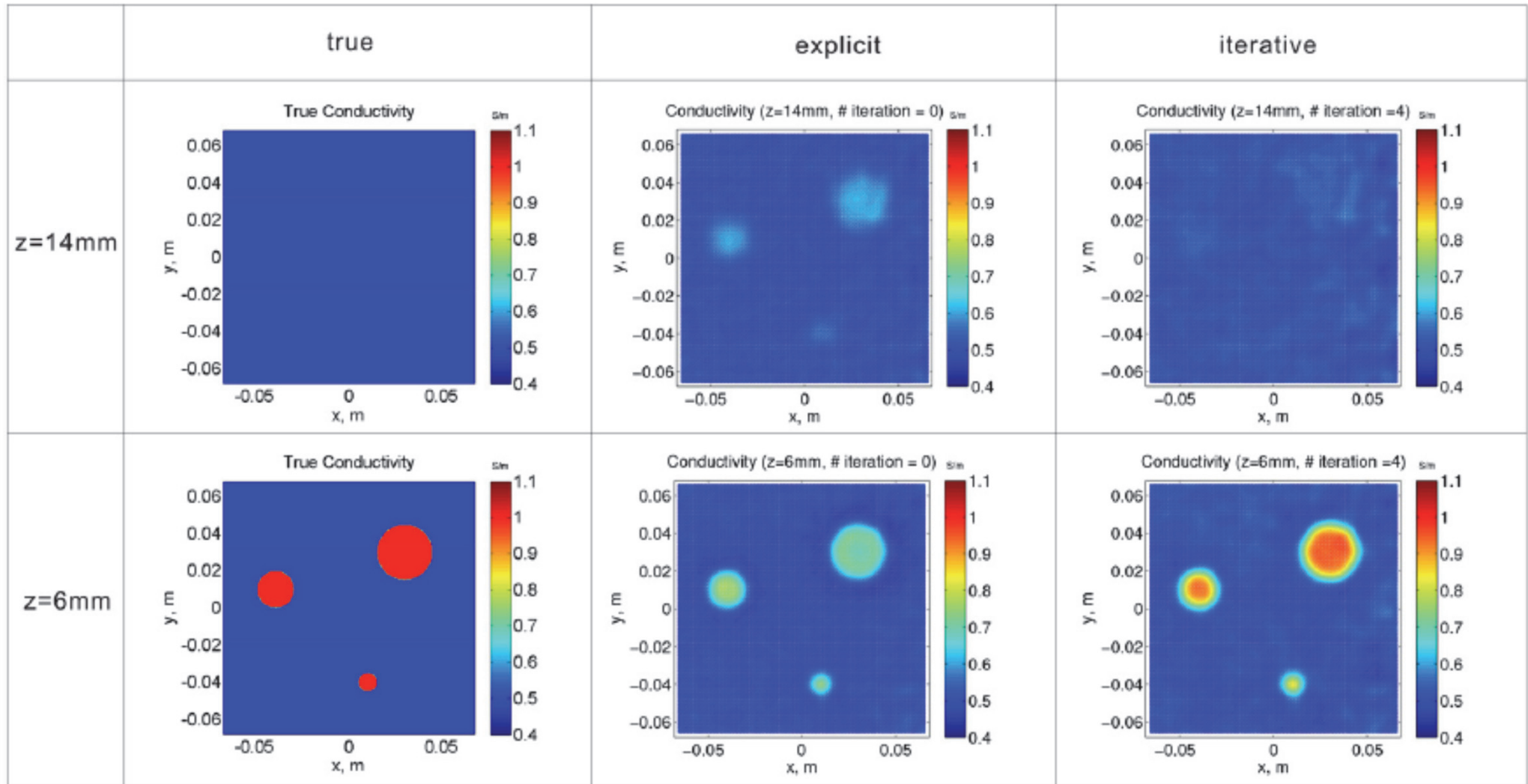
# Numerical simulations

- 64MHz, plane wave input
- Z-axis sampling: 2mm
- $\partial_z E^+$  : central difference
- Gaussian filter: 3x3x3, sd=1pixel
- Convergence criteria:

$$\sqrt{\frac{1}{M} \sum_{i=1}^M |\gamma^{(n+1)}(\mathbf{r}_i) - \gamma^{(n)}(\mathbf{r}_i)|^2 / |\gamma^{(n)}(\mathbf{r}_i)|^2} < c = 10^{-5}$$



# Noise 1%



# Concluding remarks

- Cauchy-Riemann equations: for potential fields
- Inhomogeneous Cauchy-Riemann equations: for the dual quantities in time harmonic wave fields
- E and H of the 2D time-harmonic Maxwell equations satisfy the  $\bar{D}$  equation, which provides a tool for computation of the unmeasurable E from the measurable H, and is thus used for reconstruction of the electric properties.
- The proposed complex-analysis-based method gives a foundation of an iterative algorithm for the 3D MREPT problem.